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THE TEARING OF WEATHERED RUBBER-COATED FABRICS

by

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#### SUMMARY

The wing-rip tear strengths of a nylon and of a cotton fabric, each coated with natural rubber, neoprene, polyurethane or chlorosulphonated polyethylene and exposed to various weathering conditions, were determined.

The coated nylon fabrics had higher tear strengths than the cotton ones, but were more variable. Polyurethane-coated nylon increased in tear strength on exposure at two Australian sites, but natural rubber coated cotton decreased on exposure in UK. Load during exposure reduced the tear strengths of the natural rubber coated fabrics.

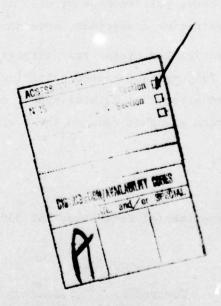
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### 1 INTRODUCTION

The exposure of rubber-coated fabrics for up to one year of weathering and the effects of this on their flexibilities, strengths and breaking extensions have previously been reported 1,2.

In a collaborative trial involving several Establishments of MOD(PE) and the Joint Tropical Research Unit (JTRU), nylon and cotton base fabrics of similar mass per unit area were coated with natural, neoprene, polyurethane (PU) or chlorosulphonated polyethylene (CSPE) rubbers. These coated fabrics were exposed for three, six or twelve months, and a second period of six months (6S) commencing at the end of the first, under loads of 1% or 10% of the nominal breaking strengths. Pieces of fabric were positioned at 45° to the horizontal and facing the equator at a site in the UK (PERME, Waltham Abbey, referred to as ERDE in the earlier reports) and at two sites in Queensland (hot, dry at Cloncurry and hot, wet, cleared jungle at Innisfail).

The coated nylon fabrics were found to be thicker, heavier and less flexible than the coated cotton fabrics; PU rubber, particularly on nylon, stiffened more than the other rubbers during exposure. The coated nylon fabrics were stronger and more extensible than the cotton ones, but those coated with natural rubber lost strength and extension at a faster rate when exposed under load. Nylon coated with PU was initially stronger and more extensible than when coated with the other rubbers, but lost these properties faster at Innisfail. Extension was more severely affected than strength by load during exposure.

The present Report gives the results and their analyses for the wing-rip tear strengths of these coated fabrics on weathering.

### 2 DETERMINATION OF TEAR STRENGTHS

The wing-rip tear strengths, the preferred British Standard method at slow speeds, were determined in accordance with the standard<sup>3</sup>, except that the rate of jaw separation was 5 cm/min instead of 10 cm/min and that only two test pieces were available per condition, both for tearing across warp threads, instead of five (except in the original controls, though to maintain uniformity in the subsequent processing of the results, the first two recorded were those used).

A 15cm cut was made across the warp in each test piece, of which the dimensions were 12.5 cm warpway × 20 cm weftway. Lines at angles of 55° to the

cut were marked on both tails, which were then inserted into the jaws of a recording tensile testing machine, with the marks along the edges of the jaws; the machine was situated in a room at 20°C and 65% relative humidity and test pieces were conditioned in this atmosphere for at least 24 h before testing. Ignoring the first peak in each tear trace, the median and maximum forces were recorded.

Most specimens gave satisfactory tears, except that in eight cases, where the tear strength was high, there was thread slippage or coating flaking. Nevertheless, tear values were obtained in all cases, and these were used in the subsequent analyses.

The uncoated cotton fabric had a median tear strength of 5.1 N, and a maximum of 7.1 N. The uncoated nylon fabric had a median tear strength of 100 N, and a maximum of 255 N.

### 3 ARRANGEMENT OF RESULTS

The median and maximum tear strengths for each condition are given in Tables 1 and 2 respectively, the duplicate results referring to replication. The determinations were inevitably separated in time of determination by well over a year, and some were not made until more than two years after the end of the exposures. The effect of this on the conclusions is not known.

As noted previously 1,2, the three month specimens from Australia were not differentiated as to their loading conditions; the columns containing the lower nylon/natural rubber tear strengths were therefore ascribed, as with breaking strength, to the 10% loading.

The tear strengths were divided into the same nine sets as for the breaking strengths<sup>2</sup>, it not being possible to consider the results as a whole because of specimen losses. Since the median and maximum tear strengths were closely correlated (correlation coefficient = 0.996, slope = 1.18), only median strengths were analysed in detail. The 368 usable values were analysed by computer using the following columns from Table 1:

Set	No.of columns in set	Columns from Table 1 used	Brief description 1
(a)	2	A, B	Controls
(b)	6	C, D, K, L, S, T	3 months
(c)	12	C, E, G, I, K, M	17
		0, Q, S, U, W, Y	
(d)	24	C-Z	Natural rubber
(e)	8	C-J	PERME
(f)	6	A, B, C, E, G, I	PERME, 1%, with controls
(g)	6	A, B, K, M, O, Q	Cloncurry, 17, with controls
(h)	6	A, B, S, U, W, Y	Innisfail, 1%, with controls
(i)	24	C-Z	Nylon with 3 rubbers

However, because the variability of the nylon fabrics was significantly greater than that of the cotton (see section 4.1), the analysis of variance assumption that the error was randomly-distributed over all the results was strained. Thus significant cotton effects could be missed, and unjustifiably significant conclusions might be drawn for the nylon fabrics. The nylon and cotton results were therefore treated separately, though the combined analysis was also performed for additional effects not obtainable in the separate analyses, making 24 altogether (3 × 8 + set (i) which contained only nylon - nylon results from set (d) which were obtainable from set (i)).

#### 4 RESULTS AND DISCUSSION

### 4.1 Analysis of errors

The variances, standard deviations and degrees of freedom of the errors are given in Table 3. The nylon/cotton error variance ratios were significant in all the sets, necessitating separate analyses (see section 3). There was little evidence for differences in variability between the sets, however: for nylon, the highest variance ratio was 3.8 for (g)/(e); and for cotton, 4.4 for (a)/(b).

The means and coefficients of variation are also given in Table 3. Both measures were smaller for cotton than for nylon. Overall, the coefficients for tear strength were slightly higher than for breaking strength but as there were no separate analyses for nylon and cotton breaking strengths, separate comparisons could not be made.

## 4.2 Analysis of median tear strengths

### 4.2.1 General

Variance ratios derived from analysis of variance within each set are given in Table 4. The effects are discussed below in their order of occurrence in the tables, it not being possible to base them on order of importance because this differed widely in the various sets. Only those effects which had better than 99.9% probability of being correct were considered.

The means of the median tear strengths for each effect are given in Table 5. These are given complete, since it was found that most were important in at least one set, and it was felt that there might be confusion if results were omitted in some cases.

The differences between pairs of means required for significance at 99.9% probability are given in Table 6.

The variance ratios in Table 4 for the interactions of fabric with the other factors were obtainable only from the overall analyses. The means in Table 5 for the fabric interactions were those from which the effects for the individual base fabrics were derived.

## 4.2.2 Effect of fabric (F)

This was obtainable only from the overall analysis. The variance ratios were upwards of 500, with the coated nylon fabrics always having higher tear strengths than the cotton: this tear strength ratio in set (a) was 5.4; in sets (c), (g) and (h), which included the longer exposures and the Australian sites, it rose to about 7 (of FT and FS below).

## 4.2.3 Effect of rubber (R) and fabric x rubber interaction (FR)

These were important in all the sets except (a) and (i). The effect on the nylon-based fabrics was greater than for the cotton ones in sets (c), (g) and (h), and greater for cotton than for nylon in sets (b), (e) and (f). This was due mainly to an increased tear strength on weathering for the PU-coated nylon, particularly at the Australian sites, and a decreased tear strength on weathering for natural rubber coated cotton at PERME (cf RS and TS below). Because the coating tended to come off the weathered PU-coated nylon during the tear tests, its tear strength approached that of uncoated nylon (section 2).

## 4.2.4 Effect of time (T) and fabric × time interaction (FT)

These were important in all sets except (a) and (i). In sets (d), (e) and (f) there was a tendency for tear strength to decrease with time, because of the

effect on natural rubber coated cotton, particularly at PERME; in sets (c), (g) and (h), there was a tendency to increase, because of the effect on PU-coated nylon, particularly at the Australian sites (cf RS and TS).

## 4.2.5 Effect of load (L) and fabric x load interaction (FL)

In set (b), ie at short times, these were of no importance, but in (d), (e) and (i) the higher load caused some significant loss of tear strength in the nylon fabrics.

## 4.2.6 Effect of site (S) and fabric × site interaction (FS)

In set (b), the coated nylon fabrics at Cloncurry had lower tear strengths than at the other sites; with set (c), the coated nylon fabrics had higher tear strengths at Cloncurry and Innisfail than at PERME, this being due to the effects on PU-coated nylon at the longer times. For set (d), the natural rubber coated nylon fabrics were not significantly affected by the site, but the natural rubber coated cotton at PERME suffered losses in tear strength. In set (i), which did not include PU or cotton, there was no significant effect of site (cf RS).

# 4.2.7 Rubber × time interaction (RT) and fabric × rubber × time interaction (FRT)

In sets (a) and (i) these were of little importance. However, in (c), the PU-coated nylon fabric increased in tear strength with time of exposure, whilst the natural rubber coated cotton fabric decreased. In sets (e) and (f), the natural rubber coated cotton also decreased in tear strength with time. With sets (g) and (h), the PU-coated nylon increased in tear strength with time.

# 4.2.8 Rubber × load interaction (RL) and fabric × rubber × load interaction (FRL)

These were testable only in set (b), where they were not significant, and (e), where the natural rubber coated nylon and cotton fabrics under 10% load had lower tear strengths than when exposed under 1% load.

## 4.2.9 Rubber × site interaction (RS) and fabric × rubber × site interaction (FRS)

In set (b), the PU-coated nylon had higher tear strength at PERME and Innisfail. With (c), the PU-coated nylon had higher tear strength at Cloncurry and Innisfail, whilst the natural rubber coated cotton had lower tear strength at PERME.

# 4.2.10 Time × load interaction (TL) and fabric × time × load interaction (FTL)

In set (d), the natural rubber coated nylon fabric under 10% load lost tear strength with time. The effects were not significant in sets (e) and (i).

# 4.2.11 Time × site interaction (TS) and fabric × time × site interaction (FTS)

In set (c), the coated nylon fabrics increased in tear strength with time at the Australian sites. In set (d), the natural rubber coated cotton fabric lost strength with time. The effects were not significant in set (i), which did not include PU or cotton.

## 4.2.12 Load × site interaction (LS) and fabric × load × site interaction (FLS)

In set (b), ie at short times, these were not significant. With set (d), the natural rubber coated cotton fabric at PERME, and, in sets (d) and (i), the natural rubber coated nylon fabric at PERME and at Cloncurry, lost more tear strength after exposure under the higher load.

# 4.2.13 Rubber × time × site interaction (RTS) and fabric × rubber time × site interaction (FRTS)

In set (c), the PU-coated nylon increased in tear strength with time at the Australian sites, and the natural rubber coated cotton lost more strength with time at PERME than at the other sites. The effect was not significant with set (i), there being no PU and no cotton.

### 4.2.14 Other interactions

The other testable interactions were: RTL and FRTL in sets (e) and (i), TLS and FTLS in sets (d) and (i), LSR and FLSR in sets (b) and (i), and RTLS in set (i). Some of these just reached significance at 99.9% probability, but they did not add appreciably to the information gained from the experiment.

#### 5 CONCLUSIONS

- (1) The wing-rip tear strength of nylon and cotton fabrics of similar mass per unit area and coated with natural, neoprene, PU or CSPE rubbers have been determined after exposure to weathering in UK or Australia for up to one year under a load of 1% or 10% of the nominal breaking load.
- (2) The ratio of tear strengths for the nylon to the cotton fabrics was more than 5, but the nylon had greater variability.

- (3) The tear strength of the PU-coated nylon increased with time at the Australian sites, due to failure of the coating permitting yarn slip and bunching.
- (4) The tear strength of the natural rubber coated cotton decreased with time in UK.
- (5) The tear strengths of the natural rubber coated nylon and cotton were lower after exposure under the heavier load, especially after longer times of exposure.
- (6) Fabrics coated with CSPE were least affected by weathering.

### Acknowledgment

The authors thank Mr D.E. Lloyd of Mathematics and Computation Department, RAE, for discussions and the arranging of the computer programs.

Table 1

Controls	9	A STATE OF THE REAL PROPERTY.		E1	MEDIAN		<b>4</b>		CH TOWAY TO	1			Tag l	Cloncurry		WALED WALED		LABRICS		1	=	imi sfail		1	
Original Final 3 6	8.	8.		9			12		89				9		12		8				9		12		S9
1 10 1 1	-	-	-	-	-	0	-	10	-	0	-	9	-	5	-	9	-	9	1 10		6	-	10	-	10
3 0 0 8 V	0 o	0	_	w		L	9	=	-	7	×	-	=	=	0	-	0	œ	S	n .	^	-	*	λ.	2
24.5 21.8 23.5 22.8 25.9 18.8 22.0 15.7 24.5 22.8 23.2 18.1	23.5 22.8 25.9 24.5 22.8 23.2	22.8 25.9 22.8 23.2	23.2	th.	8 8		23.5	13.3	22.0 27	21.2 18	18.4 17 25.9 19	19.6	22.9	19.0 32. 18.8 37.	29.58	13.7 25	25.1 <sup>a</sup> 19.1 30.2 <sup>a</sup> 21.6	.1 22.8	.8 22.8	16.1	18.4	19.6	18.1	26.3	23.9
25.9 20.8 22.6 23.5 22.4 19.6 25.1 22.6 22.8 22.8	22.6 23.5 22.4 22.4 21.2 22.6	23.5 22.4 21.2 22.6	22.4		19.6		24.9 2	22.8 18	18.8 27	20.4 21	19.2 20	20.4 21	21.6 2	23.5 22	22.0 21	25.5 25	20.6 21	21.6 24.3	3 22.0	2 22.0	3 25.9	22.4	30.4	22.6	25.7
29.0 24.9 28.4 27.7 25.1 25.9 29.4 22.8 28.8 29.0 26.3 27.9	28.4 27.7 25.1 28.8 29.0 26.3	27.7 25.1 29.0 26.3	25.1		25.9		24.7	24.3	25.9 27	27.5 21	21.2 18	18.8 27	27.9	9 68	89.8ª	55.	52,5ª	22	23.2 33.0	8 77.5 0 80.4	5 83.4b	b 71.6a b 75.0a	, ,	57.4	• •
22.4 23.1 23.3 23.2 20.8 20.0 24.3 23.5 23.2 22.0 23.9 21.2	23.2 22.0 23.9	23.2 20.8 22.0 23.9	23.9		20.0		20.4 2	22.0	21.2	22.0 23	23.2 23	73.5 23	23.5 2	21.6 20	20.8 22	22.8 23.0 23	23.7 22	22.6 22.0	0 26.7	7 23.5	5 22.8 9 22.8	24.0	23.5	23.1	23.5
4.5 4.6 4.3 4.2 3.1 3.1 4.7 4.7 4.4 4.3 2.9 2.9	4.3 4.2 3.1 4.4 4.3 2.9	4.2 3.1	3.1		3.1		1.8	0.5	3.9	3.3	5.5	4,5	3.9	6.3	3.8	3.2	E + +	3.9	4.3 4.3	3 3.9	3.9	3.9	3.5	33	4.5
4.7 4.8 4.6 4.4 4.1 4.3 4.6 4.7 4.8 4.6 4.1 4.1	4.6 4.4 4.8 4.6 4.1	4.6.4	22		5.2		3.9	-5.5	1.3	3.9	3.9	6.3	3.7		3.4		3.8	3,6	3.9 4.3	3.7.	3.9	3.5	• •	3.9	3.8
4.0 4.0 4.1 4.2 3.9 3.9 4.3 4.7 4.0 4.0 3.9 4.1	4.1 4.2 3.9 4.0 4.0 3.9	4.2 3.9	3.0		3.9		3.5	3.3	3.5	3.5	3.7	3.5	3.9	3.9	33	, + m	3.8	4.4.	3.9 3.9	3.9		3.6	3,5	37	4.6
3.9 4.0 3.7 3.6 4.1 3.9 4.3 3.9 4.3	3.7 3.6 4.1	3.6 4.1	7 3.9		64		3.7	3.5	3.8	3.9	3.9	3.7 3	3.3		3.7	m'm'	3.5	3.5	3.9 3.7	7 3.9	4.3.	3.4	33	3,5	33

- specimen lost or damaged

a thread slippage

b coating flaked

Table 2

	Controls	sle		되	MAXIMUM	11 0	TEAR		STRENGTHS,		Z	OF L	WEAT	WEATHERED	11 >	COATED		FABRICS	81			Inni sfail	=			
Original Fi	-	Final		9		9	12		68		е .		6		12		88		~		9	-	12	-	8	
			-	10	1	10	-	10	-	10	-	9	-	01	-	10	-	0	-	6	-	9	-	9	-	5
Y		8	ပ	0	3	L	9	Ŧ	_	7	×	-	*	2	0	a	0	œ	8	-	9	>	-	*	>	2
	- 10											3									-	-		$\vdash$	-	
Natural 31.8 31.4	Territoria.	27.3	29.8	27.5	29.9	29.1	30.7	17.2	29.0 2	25.2 2	34.3	22.1	24.7	25.7 23	>39.2ª	19.8	35.7ª 2	23.1 30	30.0 30	25.1 2	23.9 23	22.1 25	25.3 20	22.0 31	31.2 2	27.9
Neoprene 32.8 29.9		27.5	31.4	32.4	26.3	25.2	28.9	29.0	26.3 2	26.2 2	26.0 3	28.9	26.9	28.5	30.8	24.9 2	25.3 2	25.7 29	31.5 26	26.4 27	27.0 31	33.0 28	28.3 33	33.7 26	26.0 29	29.6
29.0		29.4.	26.1 36.9	35.3	34.8	34.2	34.8	33.6	38.7 3	32.4 3	30.4 2	22.3	34.1	1 1	94.2ª		61.3ª 67.7ª		31.0 40	38.0 86	87.9 <sup>b</sup> 104.0 <sup>b</sup> 89.1 <sup>b</sup> 95.7 <sup>b</sup>	.06 80.	80.9ª	8 3	e	
28.9		28.7	28.6	26.9	8.3	23.7	25.8	24.9	25.7 2	28.1	20.2	23.5	23.4	25.8	26.5 2	26.9 2	28.3	25.9 2	29.4 28	28.3	29.4 28	28.6 29	29.9 28	28.0 30	30.4 20.92	28.0
Natural 5.7		5.9	5.9	6.2	4.2	9:4	2.6	1.0	5.3	5.2	6.2	5.8	5.3	5.7	. 4.9	5.0	5.3	5,5	6.2	5.8	5.6	5.6 5	5.3	5.0 6	6.0	6.1
Cotton Neoprene 6.1		6.0	5.9	6.3	6.0	6.2	5.8	6.9	6.2	5.5	5.4	6.0	8.8	••	5.2	• •	5.6	5.0	5.7	6.0	5.0	5.5	5.2		4.5.	5.5
5.9		8.8	5.6	5.7	5.3	6.5	5.3	4.5	5.0	5.5	5.3	5.2	5.8	5.4	5.6	• •	5.1	6.4	4.0.	5.2	5.4	9.0	6.1	5.3	6.0	5.6
4.9	-0	5.2	5.5	5.1	5,8	3.4	5.2	5.0	5.0	5.2	5.5	5.0	9.6.		6.6	. ,	6.5	5.2	5.6	5.9	5.6	6.3	4.4	5.1	4.3	6.2
	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	+	1	1

- specimen lost or damaged a thread slippage

Table 3
ANALYSIS OF ERRORS

Property	Source					Set				
		(a)	( <b>9</b> )	(e)	(p)	(e)	(£)	(8)	(p)	(i)
Error variance Ny	Nylon	3.509	2.432	3.216	•	1.611	2.483	5.182	2.282	2.672
8	Cotton	0.0391	0.0088	0.0161	0.0350	0.0278	0.0233	0.0216	0.0255	•
Ž Š	Nylon/cotton error variance ratio	8	275	197	•	57	117	239	06	1
6	Overall	1.774	1.220	1.616	2.082	0.819	1.253	2.602	1.157	1
Set mean, N N	Nylon	23.6	33.2	28.2	,	22.9	23.6	27.6	28.7	22.2
8	Cotton	4.4	4.1	3.8	3.8	3.7	3.9	4.6	4.1	•
6	Overal1	14.0	13.6	0.91	12.6	13.2	13.7	15.8	16.4	1
	Nylon	1.874	1.560	1.793	1	1.269	1.576	2.276	1.513	1.635
deviation, N C.	Cotton	0.198	0.000	0.127	0.187	0.167	0.152	0.147	0.160	1
8	Overal1	1.332	1.105	1.271	1.443	0.905	1.119	1.613	1.075	1
of	Nylon	7.9	8.9	6.4	1	6.4	6.7	8.2	5.2	7.4
variation, % C	Cotton	4.5	2.4	3.3	6.4	4.5	3.8	3.6	3.9	1
6	Overal1	9.5	8.1	7.9	11.5	6.9	8.2	10.2	6.5	1
es of om in	Nylon Cotton	&	24	48	24	32	24	24	24	72
error	Overal1	91	48	96	48.	49	87	48	48	•

Table 4

TABLE OF VARIANCE RATIOS

Effect	Source	Degrees of	No.of	No.of results	+				Set				
Priect	source	freedom	levels	per level	(a)	(b)	(c)	(d)	(e)	(£)	(4)	(h)	(i)
,	Overall	1	2	16	1668								
7	Overall	1	2	48		7106		3625.6		840	517	1267	
7	Overall	1	2	96			18569						
	Overall	1	2	64					16958				
	Nylon	3	4	4	5.9						18		
R	Cotton	3	4	4	12.1								
R	Overall	3	4	8	5.3								
R	Mylon	3	4	12		12.8				18.9	177.7	845.9	
	Cotton	3	4	12		112.8				47.3	37.1	17.1	
R	Overal1	3	4	24		9.8			1.0	20.5	181.7	833.6	
R	Nylon	3	4	24			855.5						
R	Cotton	3	4	24		4	17.6						
R	Overall	3	4	48			912.0						
R	Nylon	3	4	16					58.2			3.75	
R	Cotton	3	4	16					150.4				
R	Overall	3	4	32					73.8				
R	Nylon	2	3	48									7.
FR	Overall	3	8	4	6.6								
TR.	Overall	3	8	12		16.5				22.8	177.7	839.2	
PR	Overall	3	8	24			897.0						
TR	Overall	3	8	16					65.3				
7	Nylon		2	8	13.5		Ŧ. 14		03.3				
	Cotton	1	2	8	1.3		- 1-			Jan 18 1			
7	Overall		2	16	12.6								
T	Nylon	,		24	12.0		128.0			N. Y			
T	Cotton	3		24			80.7						
7	Overall	3		48			114.4						
	A STATE OF THE PARTY OF THE PAR						114.4				H	ti branci	
1	Cotton	3	*	12				154.3					
T	Overall	3	*	24				11.3					
T	Nylon	3	•	16					9.2			100	
T	Cotton	3	4	16					121.4			and the second	
1	Overall	3	4	32					28.6				
T	Nylon	5	6	8						5.1	68.5	128.4	
T	Cotton	5	6	8						72.9	36.4	23.2	
T	Overall	5	6	16						8.9	93.3	118.1	
T	Mylon	3	•	36								Dane.	2.
n	Overall	1	4		14.3							1	
m	Overall	3	8	24			141.3					10.20	
77	Overall	3		12	-11			4.7					
n	Overall	3		16					6.0			200	
n	Overall	5	12	8						6.1	102.8	136.3	
L	Wylon	1	2	24	1	0.0	7,000	MAN E				100	
L	Cotton	. 1	2	24	200	0.0		5.4					
L	Overall	1	2	48		0.0		72.9				10000	
L	Nylon	1	2	32		N. Karal			17.5				
L	Cotton	1	2	32					2.9			21,000	
L	Overall	1	2	64					15.7				
L	Mylon	1	2	72		Ser View	4-71-5				TO THE REAL PROPERTY.		23.

Table 4 (continued)

		Degrees of	No.of	No.of results					Set				
Effect	Source	freedom	levels	per level	(a)	(b)	(c)	(4)	(e)	(f)	(8)	(h)	(i)
n.	Overall	1	. 4	24		0.0		65.8					
PL.	Owrell	1	4	32					12.1				
8	Nylon	2	3	16		22.1						Hered	
8	Cotton	2	3	16		10.6		189.5					
8	Overall	2	3	32		23.4		4.0					
S	Nylon	2	3	32			165.4						
8	Cotton	2	3	32			11.7					21-64	
S	Overall	2	3	64			192.1						
8	Nylon	2	3	48									3.7
78	Overall	2	6	16		20.7		4.6					
75	Overall	2	6	32			178.9						
RT .	Nylon	3	8	2	1.6								
KT	Cotton	3	8	2	0.1								
KT	Overall	3	8	4	1.5								
KT	Nylon	9	16	6			120.5						
128	Cotton	9	16	6			29.7						
RT .	Overall	9	16	12			132.4						
RT .	Nylon	9	16	4					2.2				
KT	Cotton	9	16	4					64.9				
RT	Overall	9	16	8					4.1				
RT	Nylon	15	24	2						2.2	69.2	151.6	
RT	Cotton	15	24	2						24.2	7.6	4.0	
RT	Overall	15	24	4						1.7	71.4	152.1	
RT	Nylon	6	12	12									5.6
FRT	Overall	3	16	2	1.6								
PRT	Overall	9	32	6			122.1						
PRT	Overal1	9	32	4					1.6				
PRT	Overal1	15	48	2						4.2	66.6	147.8	
RL.	Nylon	3	8	6		4.6							
RL.	Cotton	3	8	6		7.1							
RL.	Overal1	3	8	12		4.6							
RL	Nylon	3	8	8					17.8				
RL	Cotton	3	8	8					6.6				
RL.	Overall	3	8	16					26.8				
RL.	Nylon	2	6	24									43.8
TRL	Overall		16	6		4.7							
FRL	Overall	3	16	8					19.8				
RS	Nylon	6	12	4		7.4							
RS	Cotton	6	12	4		16.2							
1.5	Overall	6	12	8		7.9					100		
RS	Nylon	6	12	8			170.2					the true	
15	Cotton	6	12	8			58.0						
RS .	Overall	6	12	16			181.1					T PARTY	
RS	Mylon		9	16						2			6.0
TRS	Overall	6	24			6.9							
735	Overall	6	24	8			181.6	100					

Table 4 (concluded)

TL TL TL TL TL TL TS TS TS TS TS	Cotton Overall Nylon Overall Nylon Overall Nylon Overall Nylon Cotton Overall Nylon Overall Cotton Overall Nylon Overall	3 3 3 3 3 3 6 6 6 6 6 6 6 6 6	8 8 8 8 16 12 12 12 12 12	6 12 8 16 18 .6 8 8 16	(2)	(b)	(e)	(d) 5.8 12.9	4.7 2.5 12.8	<b>(t)</b>	(8)	(h)	(4)
IL IL IL IL IL IT IS IS IS IS IS	Overall Nylon Overall Nylon Overall Nylon Overall Nylon Cotton Overall Cotton Overall Nylon	3 3 3 3 3 3 3 6 6 6	8 8 8 16 16 12 12	12 8 8 16 18 .6 8				12.9	2.5				1.7
IL IL IL IL IT IS IS IS IS IS	Nylon Cotton Overall Nylon Overall Nylon Cotton Overall Cotton Overall Nylon Overall	3 3 3 3 3 6 6 6	8 8 16 16 12 12	8 8 16 18 .6 8 8					2.5				1.7
TL TL TL FTL FTL TS TS TS TS	Cotton Overall Nylon Overall Overall Nylon Cotton Overall Cotton Overall Nylon	3 3 3 3 6 6 6	8 8 16 16 12 12	8 16 18 .6 8 8				10.0	2.5				1.7
TL TL FTL FTL TS TS TS TS TS	Overall Nylon Overall Overall Nylon Cotton Overall Cotton Overall Nylon	3 3 3 6 6 6	8 16 16 12 12	16 18 .6 8 8				10.0					1.7
TL FTL TS TS TS TS TS TS	Nylon Overall Overall Nylon Cotton Overall Cotton Overall Nylon	3 3 6 6 6	8 16 16 12 12 12	18 .6 8 8				10.0	12.8				1.7
FTL FTL TS TS TS TS TS TS	Overall Overall Nylon Cotton Overall Cotton Overall Nylon	3 6 6 6 6	16 16 12 12 12	.6 8 8				10.0					1.7
FTL 13 15 15 15 15 15 15 15 15	Overall Nylon Cotton Overall Cotton Overall Nylon	6 6	16 12 12 12	8 8				10.0	STATE OF THE PARTY OF				
TS TS TS TS	Nylon Cotton Overall Cotton Overall Nylon	6 6 6	12 12 12	8				1000000					
TS TS TS	Cotton Overall Cotton Overall Nylon	6 6	12 12	8					3.2			-	
TS TS	Overall Cotton Overall Nylon	6	12	11 11 11 11 11			83.7					11 11 3	34.0
TS TS	Cotton Overall Nylon	6		14			14.1	100					
TS	Overall Nylon		12	10		- 4 -	98.8					4.45	
	Nylon	6		4			10.00	50.3					
-			12	8				6.9				-	-No-
10	Overal1	6	12	12									3.7
PTS		6	24	8			91.7						14
PTS .	Overall	6	24	4				5.2					
LS	Nylon	2	6			4.8	100	12.15				1	
LS	Cotton	2	6	8		3.5		8.3					
LS	Overall	2	6	16		5.2		14.4					
LS	Nylon	2	6	24			N. Deli						12.5
FLS	Overall	2	12	8		4.3		12.3					
RTL	Nylon	9	32	2					4.0				7
RTL	Cotton	9	32	2					3.0				
RTL	Overall	9	32	4					6.5				
RTL	Nylon	6	24	6									10.0
PRTL	Overall	9	64	2					4.7				
RTS	Nylon	18	48	2			70.0						
RTS	Cotton	18	48	2			14.8						
RTS	Overal1	18	48	4			75.0						
RTS	Nylon	12	36	4									3.2
	Overall	18	96	2			73.7						
TLS	Cotton	6	24	2				2.3					
TLS	Overall	6 .	24	4				5.5					The second
	Nylon	6	24	6						34 46			3.4
	Overall	6	48	2			199	5.6					35.5
	Nylon	6	24	2		5.2							
	Cotton	6	24	2	3.00	4.5							
	Overall	6	24		100	5.1							
	Nylon		18										5.5
	Overall	6	48	2		5.2							
	Nylon	12	72	2									4.1

Table 5

TABLE OF MEAN MEDIAN TEAR STRENGTHS, N

						Set				
Factor	Love? .	(a)	(b)	(c)	(4)	(0)	(f)	(9)	(h)	(1)
•	Ny lon Cotton	23.6 4.5	. 23.2 4.1	20,1 3,6	21.6 3.7	21.5 3.7	23.4 4.0	27.6 4.0	28.7	
	Hatura's Hooprone PU CSPE	12.9 14.1 15.4 13.6	13.0 13.2 14.6 13.4	13.8 12.9 24.0 13.0		12.3 12.9 15.1 12.9	13.4 13.2 15.1 13.0	14.4 13.1 22.4 13.3	12.7 13.6 25.9 13.4	21.6 22.5 22.6
R	Natural Neoprono PU CSPE	Hylon Cotton 21,0 4,6 23,5 4,7 26,5 4,3 23,3 3,9	Hylen Cotton 21.8 4.4 22.2 4.3 25.4 3.9 23.2 3.8	Hylen Cetten 23.8 3.8 22.2 3.9 44.1 3.9 22.5 3.7		Hylen Cotten 21,5 3,0 21,6 4,2 26,4 3,8 21,8 3,8	Hylen Catten 23,2 3.7 22.6 4.4 26,5 3.9 22,2 3.8	tylen Catton 24.7 4.3 22.2 4.0 40.7 4.1 23.0 3.7	Mylen Cotton 21,1 4,3 23,2 4,1 47.8 4,0 23,1 3,8	
1	Original Final 3 months 6 months 12 months 65 months	14.8 13.1		13.6 15.6 18.2 16.4	13,0 12,0 118 13,8	14.0 13.3 12.4 13.2	14.8 13.1 14.4 13.7 12.9 13.2	14.8 13.1 12.9 13.3 22.8 17.9	14.8 13.1 13.5 19.8 19.0 18.1	22.4 21.8 21.9 22.8
FT	Original Final. 3 aenths 6 months 12 months 65 months	Hylon Cotton 25,3 4,3 21,9 4,4	,	23,2 4,1 27,5 3,8 33,2 3,5 28,9 3,9	21.8 4.4 19.9 3.7 20.8 2.8 23.4 4.1	24.3 4.2 22.8 3.8 21.6 3.1 22.7 3.8	Hylon Cotton 25,3 4,3 21,9 4,4 24,6 4,2 23,7 3,7 23,5 3,2 22,6 3,8	Bylon Cotton 25.3 4.3 21.9 4.4 21.8 4.0 23.2 3.7 41.8 3.6 31.8 3.9	Nylon Cotton 25.3 4.3 21.9 4.4 23.2 4.0 35.8 3.8 34.3 3.7 32.4 4.0	
L	1% 10%		13.6 13.5		13.8 11.4	13.5 12.9				22.8 21.6
FL	1% 10%		Hylon Cotton 23.2 4.1 23.1 4.1		Hylon Cotton 23.8 3.8 19.0 3.7	Hylen Cotten 23.9 3.7 19.0 3.7				
\$	PERME Cloncurry Innisfail		14. 2 12. 6 14. 0	13.5 16.7 17.7	12.3 13.2 12.4					21.6 22.3 22.6
FS	PERME Cloncurry Innisfall		Notes Cotton 24.3 4.2 21.0 4.0 24.0 4.1	Hylon Cotton 23.6 3.7 29.5 3.8 31.4 3.9	Hylen Cotton 21.5 3.0 22.3 4.1 20.6 4.2					
RL .	Hatural Hosprono PU CSPE		1% 10% 13.7 12.5 13.3 13.0 14.0 15.2 13.3 13.5			1% 10% 13.7 10.8 12.9 12.9 15.0 15.2 12.8 12.9				1% 10% 23.8 19.0 22.2 22.9 22.5 22.6
FRL	Bylon Natural Neoprone PU CSPE		1% 10% 23.0 20.6 22.5 21.8 24.2 28.5 22.9 23.4			1% 10% 24.1 18.8 21.5 21.7 26.2 26.6 21.7 22.0				
	Cotton Natural Nooprono PU CSPE		4.4 4.4 4.2 4.4 3.9 3.9 3.0 3.7			3,2 2,8 4,2 4,3 3,6 3,6 3,8 3,8				

Table 5 (continued)

3	-		3	-			(5)				3			\$ E		-		(6)			Ξ		-	3	
		Natural	latural Heoprene PU CSPE		CSPE	Matural	Hatural Neopren	PU CSPE		Natural Neoprene	ne PU	CSPE	Natural Neoprene	leopr en e	PU CSPE		Natural Neoprene	ene PU	CSPE	Natural Neopreme	eobrese	PU CS	CSPE Natur	Natural Neoprene	ane CSPE
5 .	Original Final 3	13.9	15.1		16.7 13.6		13.3	14.0 13.				13.3	13.9	13.2			4			13.9					
929						14.6	13.1	23.6 13.7 33.5 12.3 25.0 13.0	3 10.3	12.8	444	12.8	7.51 13.34	12.2	14.8 13.1 14.1 11.7 14.7 12.6	1 12.0	12.3	3 47.6	12.0	10.6	13.4	38.6 13 31.2 13	13.8 13.1 23.4 13.3	22.22	22.8
000	Mylon Original Final	73.2	25.5		29.2 23.3								23.2	25.5						23.2	25.5		E. E.		
12						22.0	22.5	24.2 22.9 43.4 23.5 62.3 21.1	23.4 1 19.5	22.5	28.5	3.5	25.5	22.5	28.6 23.2 25.7 22.4 25.9 19.6	32.2	2.2.2	25.3	2.5.3	22.8 17.3 18.1	23.2	23.2 22 79.0 23	22.0		
+ 0 4	6S Cotton Original Final	33	22		4.1 3.9	×2.	71.6						2 27	ž 22		~	~		~	; 37	2 33	~	2. 6.0		
12 9						1227	385	9.	3.1.3	2777	33.5	33.5.3	1.6	3523	2022	3265	2222	7 8 3 6 7 6 7	3.5.6	7221	25.50	2223	9 6 6 6		

Table 5 (continued)

	l										Set									
Factor	Level		(6)	7			(c)				(d)			(0)				(1)		
RS	PERIE Cloncurry Innisful?	Natural 13,8 12,5 12,9	13,5 12,6 13,6	11.8	13,3 13,3 13,7	13.7 15.2 12.7	12.9 12.6 13.4	25.8	12.8 13.2 13.3								21.5 22.1 20.6	21.9 22.0 23.9		21.8 22.5 23.3
RIS .	Hylon PERIE Cloncurry Innisfall Cotton PERIE Cloncurry Innisfall	Hatural 23,4 20,4 21,6 4,3 4,5 4,4	22.5 20.9 23.1 6.6 6.2 6.1		23.0 22.9 23.6 3.7 3.8	Heture) 24,1 26,5 21,2 3,2 4,1 4,1	22.1 21.5 23.1 4.2 3.7 3.8	47.8 58.4 3.8	21.7 22.9 23.0 3.8 3.5 3.7											
R	1½ 10½									3 13.7 12.5	6 12.2 11.3	12 6S 14.6 14. 9.0 12.	14.4		12 12.9 11.8	6\$ 13.2 13.2	3 22.8 21.9	6 22.4 21.2	12 23.2 20.8	6\$ 23.2 22.3
FIL	Hylon 1% - 10% Cotton 1% 10%									3 23.0 20.6	6 21.1 18.7 3.6 3.8	- 12 6S 26.1 25.1 15.4 21.1 3.0 4. 2.6 4.0	24.0	21.8	12 22.6 20.6 3.2 2.9	3.8				
TS	PERME Cloncurry Innisfail					3 14.4 12.9 13.5	6 13 8 13.3 19.8	22.8	6\$ 13.2 17.9 18.1	3 13.8 12.5 12.9	6 12.3 12.2 11.0	12 6S 10.3 12. 14.2 14. 11.0 14.					3 23.0 21.4 22.8	6 21.6 21.0 21.8		6\$ 21,5 22,9 23,8
FTS	Hylon PERME Cloncurry Inntafatl Cotton PERME Cloncurry Inntafatl					3 24.6 21.8 23.2 4.2 4.0 4.0	6 23,8 23,2 35,8 3,8 3,8	41.9	3,9	3 23.4 20.4 21.6	6 21.5 20.2 18.1 3.0 4.2 3.9	12 6S 19.5 21.4 24.7 24.1 18.1 24.1 1.1 3. 3.6 4. 3.9 4.4								
LS	PERIE Clencurry Innisfall	14	1.4 1.9 1.5	14	1.1 2.2 3.5					1% 13, 15, 12,	2	10% 10.8 11.0 12.7					22	1 .5 .6	20	7.8 1.9
FLS	Hylon PERME Cloncurry Inntafall Cotton PERME	21 21	1.6 1.8 1.2	20 20	12 0.0 0.3 0.9					1½ 24, 26, 21,	5 2	10% 18.8 18.0 20.2								
	Clencurry Innisfail		.0		.1					4.	1	4.0								

Table 5 (continued)

7	[0,00]				Š	Set			
ractor			٦	(e)				Ξ	
RTL	ħ	3	9	12	65	3	9	12	68
	Natural	14.2	13.8	13.4	13,3	23.0	21.1	26.1	25.6
	Neoprene	13.6	13,3	12.3	12.3	22.5	22.5	22.4	21.6
	2	16.4	14.8	14.1	14.8				
	CSPE	13.5	13.2	11.7	12.6	22.9	23.5	21.1	22.5
	107								
	Natural	13.5	10.8	7.2	12.0	20.6	18.8	15.4	7.12
	Neoprene	13.4	12.8	13.3	12.5	21.8	23.3	24.4	22.7
	2	16.3	15.5	14.1	15.2				
	CSPE	13.1	12.4	12.7	13.5	23.4	21.5	22.6	22.9
FRIL	Nylon 1%								
	Natural	24.0	24.5	25.3	22.8				
	Neoprene	22.5	22.6	23.2	20.2				
	2	28.6	25.7	25.9	25.9				
	CSPE	23.2	22.4	19.6	21.4				
*	Nylon 10%								
	Natural	22.8	18.4	13.7	20.4				
	Neoprene	22.4	21.2	22.4	8.02				
	2	78.4	56.9	24.7	26.5				
	CSPE	22.6	20.6	21.6	23.2				
	Cotton 1%								
	Natural	:	3.0	1.6	3.9				
	Neoprene	4.7	4.1	3.9	4.2				
	2	4.1	3.9	3.6	3.6				
	CSPE	3.7	4.0	3.7	3.7				
	Cotton 10%								
	Natural	4.3	3.0	0.5	3.5				
	Neoprene	4.5	4.2	4.2	7				
	2	4.1	4.0	3.4	3.8				
	Cope	11	4 4	2 2					

Table 5 (continued)

Factor	Level	Set							
ractor	Level			(c)				(1)	
RTS	PERME	3	6	12	6\$	3	6	12	6\$
	Natural	14.2	13.8	13.4	13.3	23.4	21.5	19.5	21.6
	Neoprene	13.6	13.3	12.3	12.3	22.5	21.9	22.8	20.5
	PU	16.3	14.8	14.1	14.8				
	CSPE	13.5	13.2	11.7	12.6	23.0	21.5	20.6	22.3
	Cloncurry								
	Natural	13.3	12.1	19.3	16.0	20.4	20.2	24.7	24.0
	Neoprene	12.3	12.7	12.3	13.3	20.9	22.6	22.2	22.3
	PU CSPE	12.4	14.6	47.6	28.9	200	00.0	~ ~	20 6
		13.6	14.0	12.0	13.2	22.9	22.9	21.8	22.5
	Innisfail	42.5	40.0						
	Natural Neoprene	13.5	10.6	11.1	15.4	21.6	18.1	18.1	24.8
	PU	13.5	41.5	38.6	31.2	23.1	24.1	25.2	23,4
	CSPE	13.0	13.8	13.2	13.3	23.6	23.2	23.1	23.2
						20.0			
FRTS	Nylon								
	PERME								
	Natural	24.0	24.5	25.3	22.8				
	Neoprene	22.5	22.6	23.2	20.2				
	PU	28.6	25.7	25.9	25.9				
	CSPE	23.2	22.4	19.6	21.4				
	Cloncurry								
	Natural	22.2	21.4	34.8	27.7				
	Neoprene PU	20.4	21.6	21.1	22.9 54.0				
	CSPE	23.3	24.5	20.7	22.8				
	Innisfai)								
	Natural	22.8	17.3	18.1	26.4				
	Neoprene	24.5	23.2	22.9	21.6				
	PU	23.2	79.0	73.4	58.2				
	CSPE	22.0	23.7	22.9	23.2				
	Gotton								
	PERME								,
	Natural	4.4	3.0	1.6	3.9				
	Neoprene	4.7	4.1	3.9	4.2				
	PU	4.1	3.9	3.6	3.6				
	CSPE	3.7	4.0	3.7	3.7				
	Cloncurry								
	Natural	4.5	4.0	3.7	4.4				
	Neoprene	4.0	3.7	3.4	3.8				
	PU CSPE	3.7	3.8	3.1	3.9				
		3.0	3.3	3.1	3.0				
	Innisfail Natural	4.3	3.8	3.9	4.4				
	Neoprene	3.9	3.7	3.7	4.0				
	PU	3.8	3.9	3.8	4.3				
Total According	CSPE	4.0	3.9	3.6	3,5				

Table 5 (continued)

Factor		Set							
ractor	Level			(d)			(	1)	
		3	6	12	6\$	3	6	12	68
TLS	17								
	PERME	14.2	13.8	13.4	13.3	23.2	23.2	22.7	21.5
	Cloncurry	13.3	12.7	19.3	16.0	22.0	22.5	25.5	24.4
	Innisfail	13.5	10.6	11.1	15.4	23.1	21.4	21.3	23.7
	10%					BOTTO F			
	PERME	13.5	10.8	7.2	12.0	22.6	20.1	19.2	21.5
	Cloncurry	11.6	11.4	9.1	12.2	20.8	21.2	20,3	21.4
	Innisfail	12.5	11.5	10.9	14.0	22.5	22.3	22.9	24.0
FTLS	Nylon 1%								
	PERNE	24.0	24.5	25.3	22.8				
	Cloncurry	22.2	21.4	34.8	27.7				
	Innisfail	22.8	17.3	18.1	26.4				
	10%								
	PERME	22.8	18.4	13.7	20.4				
	Cloncurry	18.6	18.9	14.6	20.4				
1.00	innisfail	20.4	19.0	17.9	23.2				
	Cotton 1%								
	PERME	4.4	3.0	1.6	3.9				
	Cloncurry	4.5	4.0	3.7	4.4				
	Innisfail	4.3	4.4	3.8	4.0				
	10%								
	PERME	4.3	3.0	0.5	3.5				
	Cloncurry	4.4	4.3	3.5	3.9				
	Innisfail	3.9	3.9	4.4	4.7				
			(6	)			(1	)	
LSR	1%		Neopre		CSPE	Natur		prene	CSPE
	PERME	14.2	13.6		13.5	24.1		2.1	21.7
	Cloncurry	13.3	12.3		13.6	26.2		1.5	22.9
	Innisfail	13.5	14.2	13,5	13.0	21.2	2	3.1	23.0
	10%								
	PERME	13.5	13.4		13.1	18.8	2	1.7	22.0
	Cloncurry	11.6	12.9		13.0	18.0	2	2.5	22.2
	Innisfail	12.5	12.9	18.1	14.5	21.1		4.9	23.6

Table 5 (concluded)

Factor		Level	-0	Set (b	)	
FLSR	Nylo		Natural	Neoprene	PU	CSPE
	17	PERME	24.0	22.5	28.6	23.2
		Cloncurry	22.2	20.4	21.0	23. 3
		Innisfail	22.8	24.5	23.2	22.0
	10	PERNE	22.8	21.4	20.4	22.6
		Cloncurry	18.6	21.4	28.4 18.6	22.6
		Innisfail	20.4	21.6	32.4	25.3
						20.0
	Cott					
	THE RESERVE OF THE PARTY OF THE	PERME	4.4	4.7	4.1	3.7
		Cloncurry	4.5	4.0	3.7	3.9
		Innisfail	4.3	3.9	3.8	4.0
	107					
		A PERME	4.3	4.5	4.1	3.7
		Cloncurry	4.4	4.3	3.6	3.7
		Innisfail	1 4.4	4.3	4.0	3.7
	<b></b>		+	Set (i)		
RTLS	3 months	1%	Natural			
NILS	3 months	PERME	24.0	Neoprene 22.5		CSPE
		Cloncurry	22.2	20.4		23. 2
		Innisfail	22.8	24.5		22.0
		10%	1			22.0
		PERME	22.8	22.4		22.6
		Cloncurry	18.6	21.4		22.4
		Innisfail	20.4	21.6		25.3
	6 months	1%				20.0
	o months	PERME	24.5	22.6		20.1
		Cloncurry	21.4	22.6 21.6		22.4
		Innisfail	17.3	23.2		23.7
			1	20.2		23.1
		10%	40.			-
		PERME Cloncurry	18.4	21.2		20.6
		Innisfail	19.0	23.5 25.1		21.2
			19.0	23,1		22.8
	12 months		45.	SHEET STATE		
		PERME	25.3	23.2		19.6
		Cloncurry Innisfail	34.8 18.1	21.1		20.7
			10.1	22.9		22.9
		10%				
		PERME	13.7	22.4		21.6
	Cloncurry		14.6	23.3		22.9
		Innisfail	17.9	27.5		23, 3
	65 months	1%				
		PERME	22.8	20.2		21.4
		Cloncurry	27.7	22.9		22.8
	1	Innisfail	26.4	21.6		23.2
		10%				
		PERME	20.4	20.8		23.2
		Cloncurry	20.4	21.7		22.1
		Innisfail	23.2	25.4		23.3

<u>Table 6</u>

DIFFERENCES BETWEEN MEANS, N, REQUIRED AT 99.9% PROBABILITY

						Set				
Effect	Source	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)
F	Overall	1.9	0.8	0.6	1.0	0.5	0.8	1.2	0.8	
R	Nylon	6.7	2.4	1.8		1.6	2.4	3.5	2.4	1.1
R	Cotton	0.7	0.2	0.1		0.2	0.2	0.2	0.2	
R	Overall	2.6	1.1	0.9		0.7	1.1	1.7	1.1	
FR	Overal1	5.4	2.3	1.7		1.5	2.2	3.2	2.2	
T	Nylon	4.7		1.8		1.6	3.0	4.3	2.8	1.3
T	Cotton	0.5		0.1	0.3	0.2	0.3	0.3	0.3	
T	Overall	1.9		0.9	1.5	0.7	1.3	2.0	1.4	
FT	Overall	3.8		1.7	2.9	1.5	2.6	4.0	2.6	
L	Nylon		1.7			1.2				0.9
L	Cotton		0.1		0.2	0.2				
L	Overall		0.8		1.0	0.5				
FL	Overall		1.6		2.1	1.0	V			
s	Nylon		2.1	1.6						1.1
s	Cotton		0.1	0.1	0.2					
s	Overal1		1.0	0.8	1.3					
FS	Overal1		2.0	1.5	2.5					
RT	Nylon	13.3		5.2	1	4.6	8.4	17.1	8.0	3.2
RT	Cotton	1.4		0.4		0.6	0.8	0.8	0.9	
RT	Overall	5.4		2.5		2.1	3.6	5.6	3.7	
FRT	Overal1	10.7		4.8		4.0	7.3	11.3	7.6	
RL	Nylon		4.8			3.3				2.3
RL	Cotton		0.3			0.4		1		
RL	Overall		2.3			1.5				
FRL	Overall		4.5			2.8		8)		
RS	Nylon		5.9	4.5						2.8
RS	Cotton		0.4	0.3						
RS	Overall		2.7	2.1				1.76		
FRS	Overall		5.5	4.2						
TL	Nylon		15			3.3				2.7
TL	Cotton				0.6	0.4				2.7
TL	Overall				2.9	1.5				
PTL	Overall				5.9	2.8				
TS	Nylon			4.5	"	0				3.2
TS	Cotton			0.3	0.7					3.2
TS	Overall			2.1	3.1					
FTS	Overall			4.2	7.2					
LS	Nylon		4.1	1.2	1.2					2.3
LS	Cotton		0.3		0.5					2.3
-	COLLOIL		0.3		0.5					

Table 6 (concluded)

2000						Set				
ect	source	(a)	(p)	(c)	(P)	(e)	(£)	(8)	(h)	(i)
LS.	0veral1		2.0		2.5					
FLS	Overall		3.9		5.1					
RTL	Nylon					9.2				6.5
RTL	Cotton					1.2				
RTL	Overal1					4.0				
FRTL	Overal1					8.1				
RTS	Nylon			12.7						8.0
RTS	Cotton			6.0						72
RTS	Overal1			0.9						
FRTS	Overal1			11.9						
TLS	Nylon									6.5
TLS	Cotton				1.4					
TLS	Overal1				7.2					
FTLS	Overal1				14.4					
LSR	Nylon		11.7							5.6
LSR	Cotton		0.7							
LSR	Overal1		5.5							
FLSR	Overal1		11.0							
RTLS	Nylon									15.9

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### REPORT DOCUMENTATION PAGE

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The wing-rip tear etrengths of a nylon and of a cotton fabric, each coared with natural rubber, neoprene, polyurethane or chlorosulphonated polyethylene and exposed to various weathering conditions, were determined.

The coated sylon fabrics had higher tear othersthe than the cotton ones, but were more variable. Polyurethans-coated sylon increased in tear strength on exposure at two Australian sites, but natural rubber coated cotton decreased on emosure in Rt. Load during exposure reduced the tear strengths of the natural rubber coated fabrics.